

# MAGNETIC STATE SELECTION IN ATOMIC FREQUENCY AND TIME STANDARDS

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## ABSTRACT

Atomic standards such as those based upon cesium and hydrogen rely upon magnetic state selection to obtain population inversion in the hyperfine transition levels. Use of new design approaches and improved magnetic materials has made it possible to fabricate improved state selectors of small size, and thus the efficiency of utilization of beam flux is greatly improved and the size and weight of the standard is reduced. The sensitivity to magnetic perturbations is also decreased, so that the accuracy and stability of the standard is improved. Several new state selector designs are illustrated and the application to standards utilizing different atomic species is analyzed.

## INTRODUCTION

The geometry and properties of the magnetic state selector are crucial elements in achieving beam standards of optimum performance. However, the overall design of the standard must be carefully considered to obtain the best balance of performance, reliability, and longevity. This paper gives a brief review of the factors which relate to the efficient utilization of beam flux and the optimization of the atomic beam state selection process, and also reviews some of the considerations which enter into the choice of atom for a standard. The design of quadrupole and hexapole state selectors is next discussed, and an idealized analysis of beam trajectories is presented for the different types. Finally, several small, efficient, magnetic state selectors are illustrated.

## MAGNETIC STATE SELECTORS AND BEAM STANDARD ELEMENTS

The essential features of the atomic beam standard<sup>1</sup> which relate to state selectors and atomic trajectories are illustrated in Figure 1.

| Report Documentation Page  |                                    |                                     |  | Form Approved<br>OMB No. 0704-0188                  |                                    |
|--|------------------------------------|-------------------------------------|--|---|------------------------------------|
| Public reporting burden for the collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington VA 22202-4302. Respondents should be aware that notwithstanding any other provision of law, no person shall be subject to a penalty for failing to comply with a collection of information if it does not display a currently valid OMB control number. |                                    |                                     |  |   |                                    |
| 1. REPORT DATE<br><b>DEC 1981</b>  |                                    | 2. REPORT TYPE                      |  | 3. DATES COVERED<br><b>00-00-1981 to 00-00-1981</b> |                                    |
| 4. TITLE AND SUBTITLE<br><b>Magnetic State Selection in Atomic Frequency and Time Standards</b>  |                                    |                                     |  | 5a. CONTRACT NUMBER                                 |                                    |
|  |                                    |                                     |  | 5b. GRANT NUMBER                                    |                                    |
|  |                                    |                                     |  | 5c. PROGRAM ELEMENT NUMBER                          |                                    |
| 6. AUTHOR(S)   |                                    |                                     |  | 5d. PROJECT NUMBER                                  |                                    |
|  |                                    |                                     |  | 5e. TASK NUMBER                                     |                                    |
|  |                                    |                                     |  | 5f. WORK UNIT NUMBER                                |                                    |
| 7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES)<br><b>Sigma Tau Standards Corporation,1014 Hackberry Lane,PO Box 1877,Tuscaloosa,AL,35403-1877</b>  |                                    |                                     |  | 8. PERFORMING ORGANIZATION<br>REPORT NUMBER         |                                    |
| 9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES)  |                                    |                                     |  | 10. SPONSOR/MONITOR'S ACRONYM(S)                    |                                    |
|  |                                    |                                     |  | 11. SPONSOR/MONITOR'S REPORT<br>NUMBER(S)           |                                    |
| 12. DISTRIBUTION/AVAILABILITY STATEMENT<br><b>Approved for public release; distribution unlimited</b>  |                                    |                                     |  |   |                                    |
| 13. SUPPLEMENTARY NOTES<br><b>Proceedings of the 13th Annual Precise Time and Time Interval (PTTI) Applications and Planning Meeting, Washington, DC, 1-3 Dec 1981</b>   |                                    |                                     |  |   |                                    |
| 14. ABSTRACT<br><b>see report</b>  |                                    |                                     |  |   |                                    |
| 15. SUBJECT TERMS  |                                    |                                     |  |   |                                    |
| 16. SECURITY CLASSIFICATION OF:  |                                    |                                     | 17. LIMITATION OF<br>ABSTRACT<br><b>Same as<br/>Report (SAR)</b> | 18. NUMBER<br>OF PAGES<br><b>21</b>                 | 19a. NAME OF<br>RESPONSIBLE PERSON |
| a. REPORT<br><b>unclassified</b>   | b. ABSTRACT<br><b>unclassified</b> | c. THIS PAGE<br><b>unclassified</b> |  |   |                                    |

For beam devices designed to use velocity focussing trajectories to achieve maximum efficiency, the quadrupole or the hexapole state selector may be used, depending upon the physical properties of the particular atom. Quadrupole state selectors have a magnetic field which increases linearly with radius about the beam axis, while hexapole state selector fields increase with the square of the radius.

The source for metallic atoms is an oven, and for gaseous molecular atoms an RF discharge dissociator. The atoms emerge from the source through a collimating exit hole of large length to radius ratio to conserve flux and then pass through the state selector wherein atoms in certain magnetic quantum states are caused to converge towards the axis, while others are deflected. Atoms in the desired state pass through an interaction region to a detector in the case of magnetic resonance standards, or to a storage region within an RF cavity in the case of maser standards.

#### BEAM INTENSITY FACTORS

The flux utilization efficiency is the product of several factors, the most important of which are:

$F_1$  = (Velocity Distribution)

$F_2$  = (Source Dissociation Efficiency)

$F_3$  = (Source Collimation Factor)

$F_4$  = (Magnetic Hyperfine Structure of the Atom)

$F_5$  = (State Selector Properties)

$F_6$  = (Target Distance and Aperture)

$F_7$  = (Detector Efficiency or Maser Parameters)

Figure 2 shows the normalized distribution of intensities in the beam emerging from the source as a function of velocity and temperature. For an oven source a most important consideration is that the distribution is relatively broad, and a state selector system may select atoms having considerably higher or lower velocity than the most probable, if desired. For example, in the case of cesium standards it is common practice to select velocities 50% or more lower than the peak of the distribution so as to achieve the highest line Q.

Another important result of the broad distribution is that it is not essential that the atomic state or the state selector have exact focussing properties to achieve maximum intensity, since atoms in some velocity range at a particular source emergent angle will be focussed

as long as the system is only approximately idealized.

The distribution of velocities from an RF dissociator source is much less ideal than the oven source. The distribution varies with many factors such as RF power, source bulb size and material, and the degree to which thermallization occurs before emerging. The most prominent features of a discharge source are the large population of hotter than ambient atoms, and less than perfect dissociation efficiency. For a device such as the hydrogen maser the most important functions of the state selector are to capture the largest fraction of the atoms in the right state, and most importantly, to deflect strongly the wrong state atoms.

Figure 3 shows the effect of the source collimator in conserving atoms.<sup>2</sup> This gives the intensity in an increment of solid angle emerging from the source collimator as a function of the emergent angle. It is clear that a large improvement in flux utilization may be obtained with the collimator, but a peak is reached when the radius to length ratio of the collimator becomes comparable to the state selector acceptance angle. In the case of discharge sources one must be aware that recombination may occur on the collimator wall, and in practice  $a/L$  is usually no smaller than .05.

#### MAGNETIC HYPERFINE STRUCTURE AND FORCES ON THE ATOM

Reference (1) may be referred to for most of the theoretical basis for this paper and for the experimental data on hyperfine frequencies and other atomic and nuclear data as well as for atomic and molecular beam early history. For the purposes of trajectory analysis several approximations will be made which are entirely valid within the accuracy required. Thus the nuclear magnetic moment is considered negligible in magnitude in relation to the electronic moment, angles measured normal to the beam axis are very small so that sines equal tangents equal angles in radians, and the magnitude of the  $z$  axis velocity is equal to the total velocity magnitude.

The starting point for energy and force considerations for  $J = 1/2$  atoms, which are almost invariably the ones of concern, is the Breit-Rabi equation (Reference 1, pp 80.) The force on the atom in the radially symmetric field magnitude and field gradient of the state selector is the first derivative of the energy with respect to the radius. Figure 4 is a plot of the energy levels of an atom with nuclear moment  $I = 1/2$  as a function of the magnetic field. The force on atoms with  $I$  greater than  $1/2$  and  $m = 0$  are the same, while the forces on levels with maximum  $|m|$  are the same as for the  $|m| = 1$  levels shown. The  $m = 0$  levels are usually the ones of primary interest for focussing in atomic standards.

For atomic beam magnetic resonance standards it is desirable to direct

atoms in a particular state through an interaction region to a relatively distant detector target. For a state with a permanent moment, or with  $H_1$  considerably smaller than the state selector fields, a hexapole magnet provides the desired focussing fields. However, if  $H_1$  is much greater than the state selector fields, or if some velocity dispersion is allowable in the detected atoms, the quadrupole state selector will usually provide a much more intense detected beam.

For maser standards the choice depends upon the target distance and aperture, but for the compact geometry of recent maser designs the quadrupole state selector provides very significant advantages as will be discussed later. It is seen in figure 4 that the value of  $H_1$  for a particular atom is important in considering the dynamical behavior of the atom within the state selector. Typical quadrupole tip fields at saturation are 10 kilogauss or greater, while hexapole tip fields of 7 kilogauss may be obtained.

Chart I below gives the approximate value of  $H_1$  calculated for several interesting atoms as well as other pertinent data. The calculations for this chart use data from Reference 1.

CHART I

| ATOM   | I   | $\nu_0$ GHz | $H_1$ GAUSS | $\Delta\nu/H^2$ -Hz/(Gauss) <sup>2</sup> | MULTIPLICITY |
|--------|-----|-------------|-------------|--|--------------|
| H 1    | 1/2 | 1.42        | 510         | 2,750                                    | 4            |
| Na 23  | 3/2 | 1.77        | 630         | 2,210                                    | 8            |
| Al 27  | 5/2 | 1.51        | 1,610       | 290                                      | 12           |
| Ga 69  | 3/2 | 2.68        | 2,870       | 160                                      | 8            |
| Rb 85  | 5/2 | 3.04        | 1,080       | 1,290                                    | 12           |
| Rb 87  | 3/2 | 6.84        | 2,440       | 570                                      | 8            |
| Ag 107 | 1/2 | 1.71        | 610         | 2,290                                    | 4            |
| Ag 109 | 1/2 | 1.98        | 710         | 1,980                                    | 4            |
| Cs 133 | 7/2 | 9.19        | 3,280       | 430                                      | 16           |
| Au 197 | 3/2 | 6.11        | 2,180       | 640                                      | 8            |
| Tl 203 | 1/2 | 21.1        | 22,600      | 20.6                                     | 4            |
| Tl 205 | 1/2 | 21.3        | 22,800      | 20.4                                     | 4            |

In calculating beam efficiencies it is important to note that atoms with  $I$  greater than  $1/2$  suffer a significant loss due to the multiplicity of the states. The number of ground state hyperfine levels for each atom is listed in the last column. Not only does the multiplicity reduce the percentage of atoms in the selected state, but there are serious problems with nearby ( $\Delta m = 0$ ) transitions which force one to use relatively high "C Fields" within the interaction region to maintain separation of the several resonances. For example, with cesium, one must use "C Fields" of the order of .04 Gauss or greater, while with  $I = 1/2$  atoms such as thallium, silver, or hydrogen, one may use fields as low as 100 microgauss or less if desired, and there is negligible inaccuracy due to lack of knowledge of the field or due to distortions from overlapping resonances.

#### CURVED BORE STATE SELECTORS

To make a state selector as small as possible and to maximize the acceptance angle, the magnet bore radius should ideally be as close as possible to the beam. It is possible to make such a state selector, and in addition to achieve a focussing field for certain of the magnetic quantum states. Figure 5 illustrates the geometry of this design. The state selector may be either hexapolar or quadrupolar. It is assumed in the analysis that atoms of the largest radius are near to and have a velocity vector tangent to the bore radius. The equations defining the magnet curve are also given in Figure 5. For an atom such as thallium a strong focussing action could be obtained for the (1,0) state, while the  $m = 1$  as well as the deflected states would be very "unfocussed." This is one example where a "pure" beam of (1,0) atoms could be obtained so that a "point" detector would not have a large noise flux of other atomic states.

In nearly all cases of interest it is not necessary (or practical) to use a curved bore state selector since the ideal bore dimensions are so small and the required curvature so slight. However, tapered bore state selectors can be made which give results nearly as good, and they are more practical to fabricate.

#### TAPERED BORE AND UNIFORM BORE STATE SELECTORS

Both hexapole and quadrupole state selectors with tapered bores are more efficient than uniform bore state selectors for beam resonance devices. For atoms such as hydrogen, sodium, or silver, with  $H_1$  very much less than the magnet tip field, a hexapole magnet would be the likely choice, although for selecting very cold atoms from a higher temperature velocity distribution a relatively weak, large bore, quadrupole would be used.

In most other cases a quadrupole state selector will give the best results. It should be emphasized that for all atoms emerging from

the source at a particular angle within the maximum acceptance angle there is always one velocity for which focussing occurs upon a given target. Thus if the range of focussed velocities falls within the more probable part of the velocity distribution, a very efficient selection of the desired state may be obtained. For most atoms a quadrupole state selector may be configured to obtain the best results, even though  $H_1$  is only a fraction of the magnet tip field.

Figure 6 diagrams the coordinates and defines the parameters which are used in subsequent equations for both the tapered bore and the constant bore state selectors. (For constant bore  $\alpha = 0$ )  $\theta_w^2$  is defined by the ratio of maximum potential energy the atom incurs in traversing the field from the axis to the bore tip divided by the thermal kinetic energy. It should be noted that the thermal kinetic energy of the atom in the beam,  $1/2mv^2$ , is equal to  $3/2 KT$ , and is independent of the particular atomic mass. It is assumed the state selector tip iron is saturated and the tip field is constant.

Figure 7 gives the trajectory equations for the quadrupole state selector for states which have a constant magnetic moment or in which the moment is essentially constant due to the magnet fields being generally greater than  $H_1$ . Figure 8 gives the results for other cases noted therein.

The equations given in the figures, if used with judgement, provide a good basis for approximating the best state selector type, as well as the bore radius and length, for a particular atom and detector target aperture and distance.

If desired, the equations of motion may be solved exactly for all cases. Thus, if  $W_w$  is the magnetic potential energy (derived from the Breit-Rabi equation), the differential equation to be solved is:

$$m\ddot{r} \pm \frac{dW_w}{dr} = 0 ,$$

which solves immediately for the angle  $\theta = dr/dz$ :

$$\theta^2 = \theta_0^2 \mp \frac{W_w}{(\frac{1}{2}mv^2)} .$$

From here  $r$  may be solved for by elementary means for either the hexapole or quadrupole.

The accuracy achieved by exact computation usually far exceeds the practical necessity in view of the uncertainties due to mechanical tolerances of the state selector, alignment inaccuracies, or the imperfection of the magnetic field pattern. Several papers on beam calculation methods have been published, one of which is given in Reference 3.

## STATE SELECTORS FOR HYDROGEN MASERS

The hydrogen maser and similar devices present a different problem than beam resonance devices. Traditionally, masers used hexapole state selectors which were placed a relatively large distance from the bulb, and were designed to focus atoms near the peak of the modified Maxwellian velocity distribution. This system is quite inefficient due to the small solid angle the bulb entrance subtends and the loss of the atoms in the higher temperature part of the real velocity distribution.

A quadrupole with very small bore diameter, and length to radius ratio much greater than that dictated by the peak of normal velocity distribution, will "capture" the largest possible flux of atoms from a source. Due to its small size and the small level of stray fields caused by the magnet, it may be placed within 1 cm or less of the maser shields without incurring shielding problems. Thus the state selector to bulb distance can be minimized. Typical state selector entrance maximum capture angles are .04 radians or less (much less for higher velocity atoms) thus if the bulb distance is 2 inches, a bulb entrance diameter of .16 inches will "capture" essentially all of the atoms "captured" in the state selector. Most importantly though, an atom which is in a state to be deflected and which starts out with a zero entrance angle will have a relatively large exit angle. Calculations for the small magnet indicate that essentially all of the "wrong state" atoms will not enter the bulb in the above example.

Due to the high state selection efficiency of the small quadrupole in a compact maser design, the source exit collimator diameter may be very small, and the idealization assumed in the calculations that the atom enters the state selector from a point source is closely realized. Hydrogen atom flux efficiencies 1,000 times better than obtained with early hydrogen masers are thus possible with recent maser designs.<sup>4,5</sup>

### STATE SELECTOR DESIGNS

Figure 9 is a picture showing 3 state selectors recently made at Sigma Tau Standards Corporation which are examples of the state of the art at this writing. On the left is a tapered bore quadrupole with a bore entrance diameter of .30 mm, exit diameter 1.4 mm, length 38 mm, and  $\alpha = .0145$ .

On the right in Figure 9 is a tapered bore hexapole with entrance diameter .90 mm, exit diameter 1.70 mm, length 38 mm and  $\alpha = .011$ .

In the center in Figure 9 is a very small tapered bore quadrupole with entrance diameter .46 mm, exit diameter .97 mm, length 25.4 mm and  $\alpha = .010$ . This state selector has been designed for a high flux compact hydrogen maser. The maximum diameters that may be used with this small state selector and still maintain magnetic saturation is



about 1.2 mm and the minimum, dictated by present mechanical tolerances, is about .25 mm. Within this range and with a length of 25.4 mm (1 inch) it may easily be configured to the requirements of atomic beam resonance standards using many of the different atoms described in this paper. The particular dimensions of the small state selector shown in Figure 9 are ideal for compact hydrogen masers with state selector to bulb distances of 2 inches to 8 inches or over, depending upon bulb aperture.

#### CONCLUSION

This paper illustrates that with new state selector designs and new and improved atomic beam standard configurations it is possible to achieve much more efficient use of source flux and to focus very large intensities of a variety of atoms. It is thus very possible to improve the efficiency, stability, and accuracy of existing standards or to design new standards based upon atoms which have fundamental properties which may be superior to those of standards presently in use.

#### ACKNOWLEDGEMENTS

Consideration of the optimum design of the beam optics for a small hydrogen maser<sup>4</sup> stimulated much of the work on this paper. The research and development program for the "Small Hydrogen Maser" was supported by the United States Air Force, RADC, Deputy for Electronic Technology, Hanscom AFB, MA. The author greatly acknowledges this support.

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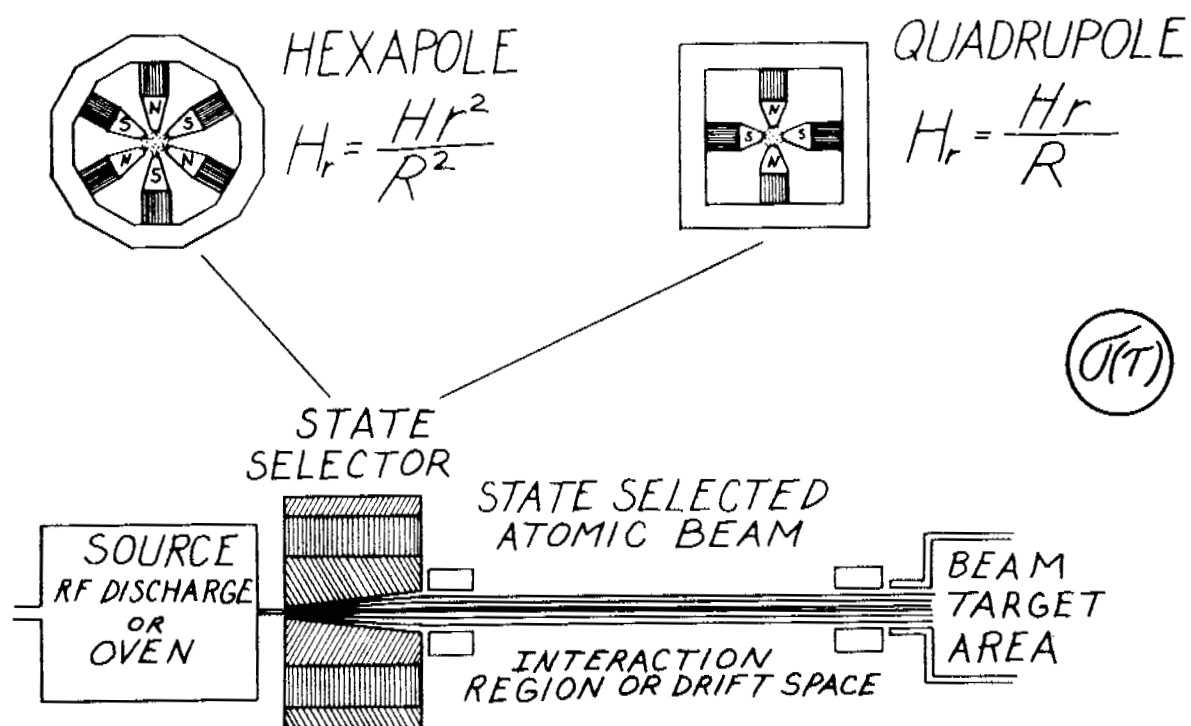


Figure 1. Magnetic State Selectors And Beam Standard Schematic.

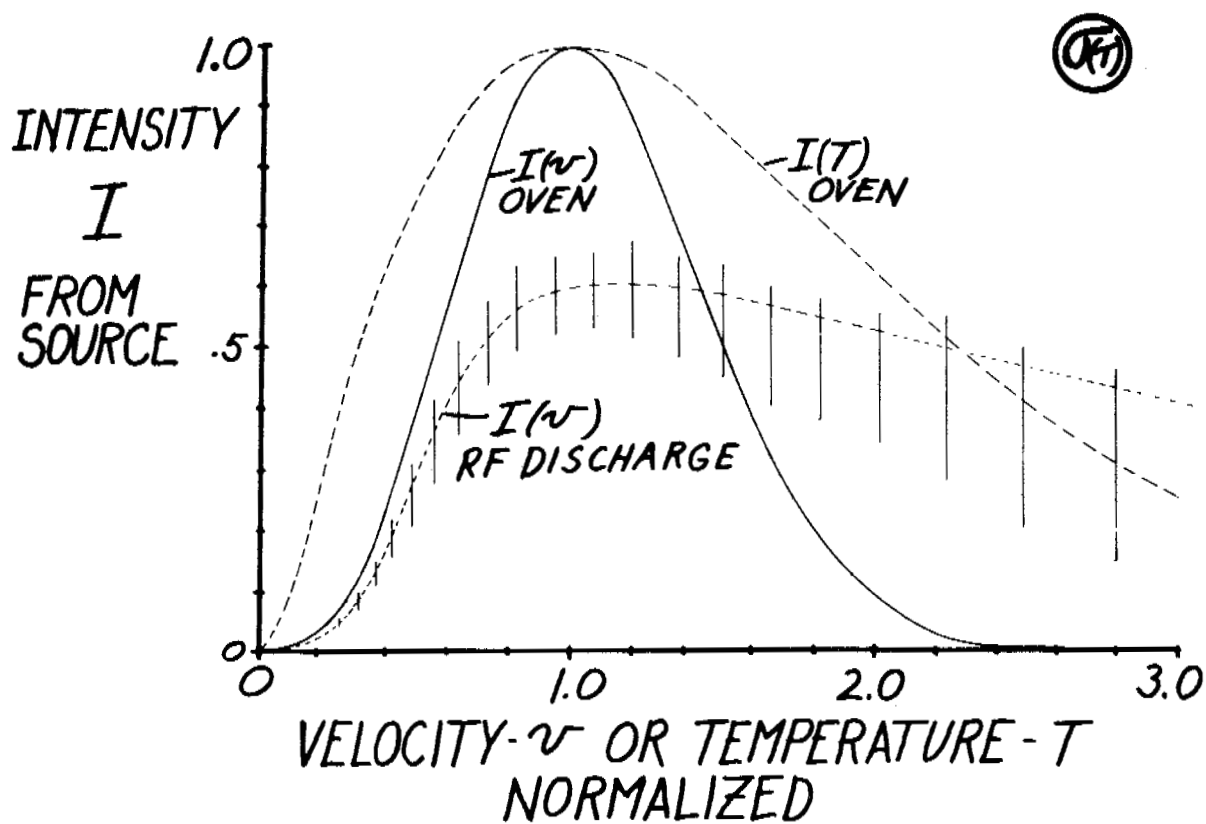


Figure 2. Intensity Distribution Of Atoms In A Beam Emerging From An Oven Or Discharge Source.

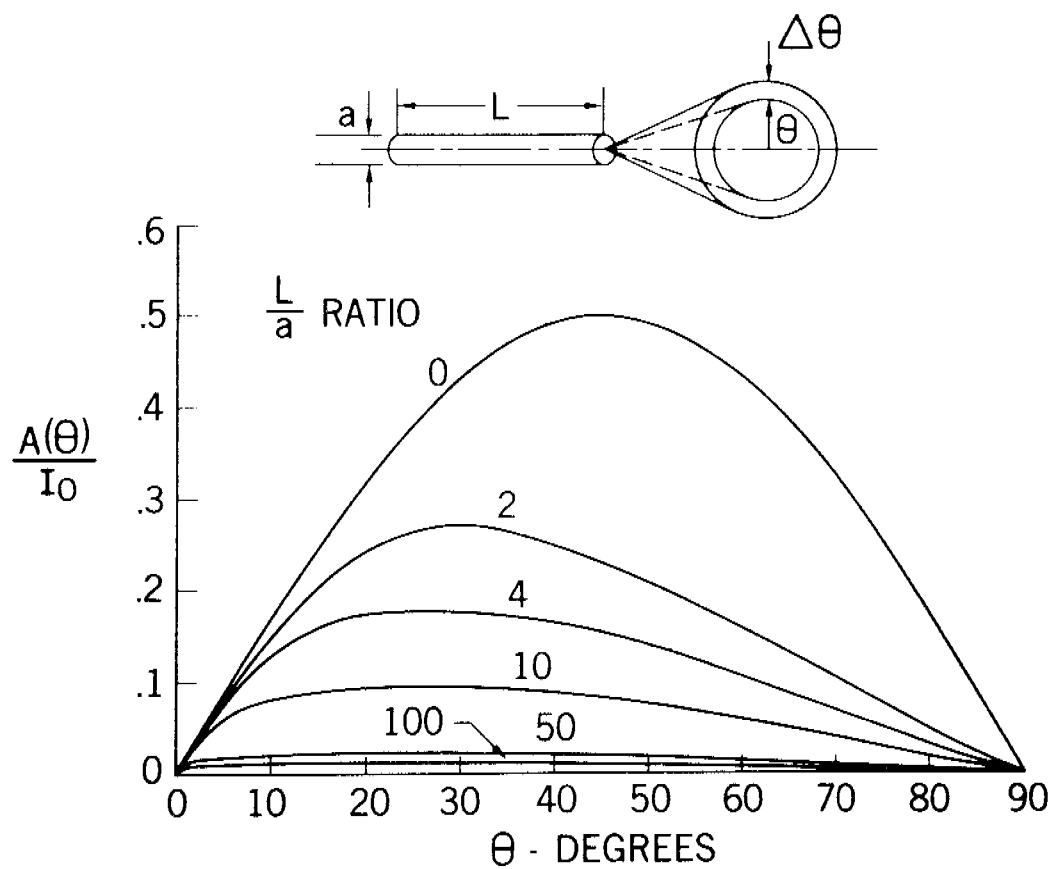


Figure 3. Intensity Of Beam In An Increment Of Solid Angle Emerging From A Source Collimator Versus The Emergent Angle.

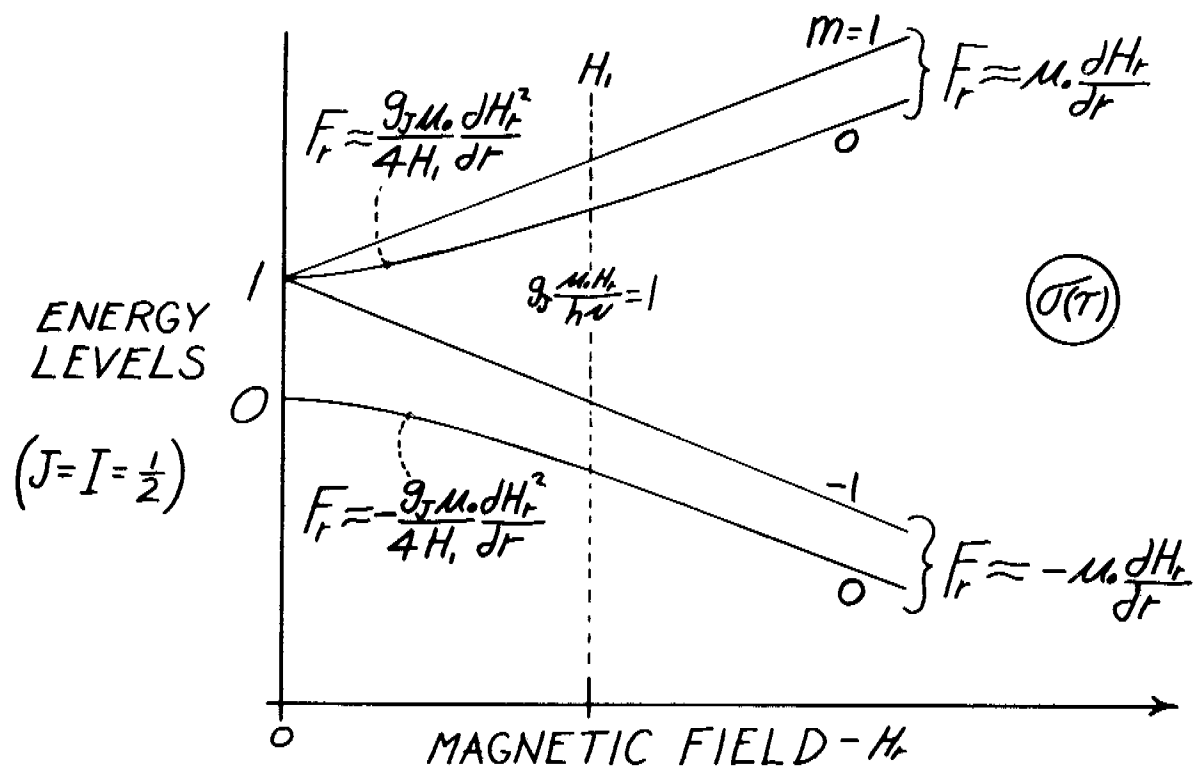


Figure 4. Magnetic Hyperfine Energy Levels Of An Atom With  $J = 1/2$  And  $I = 1/2$  Versus Magnetic Field.

$$\text{For } \Theta_L = 0, \frac{dR}{dz} = \sqrt{2} \Theta_w S$$

$$v_z \doteq v, S \equiv \sqrt{\ln\left(\frac{R_L}{R}\right)}, L_n = \frac{\sqrt{2} R_L}{\Theta_w} \int_0^S e^{-y^2} dy$$

$$\Theta_w^2 = \frac{g_J H}{4 H_1} \Theta_T^2, \Theta_T = \sqrt{\frac{\mu_0 H}{\frac{1}{2} m v^2}}$$

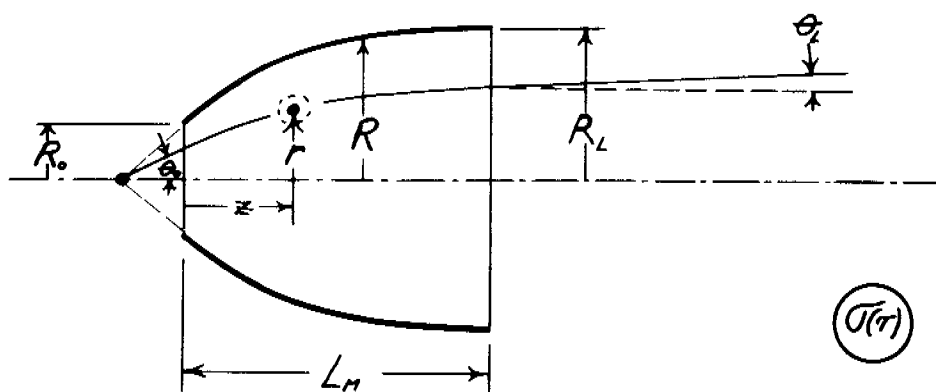


Figure 5. Curved Bore State Selector Diagram And Curvature Analysis.

$$\text{SLOPE } \frac{\Delta R}{\Delta z} = \frac{R_L - R_0}{L_M} = \alpha$$

$$R = R_0 + \alpha z$$

(U(T))

$$\Theta_0^2(\text{Max}) = \Theta_w^2 + \alpha^2$$

$$v_r = \frac{dr}{dt} \quad v_z \doteq v = \frac{dz}{dt}$$

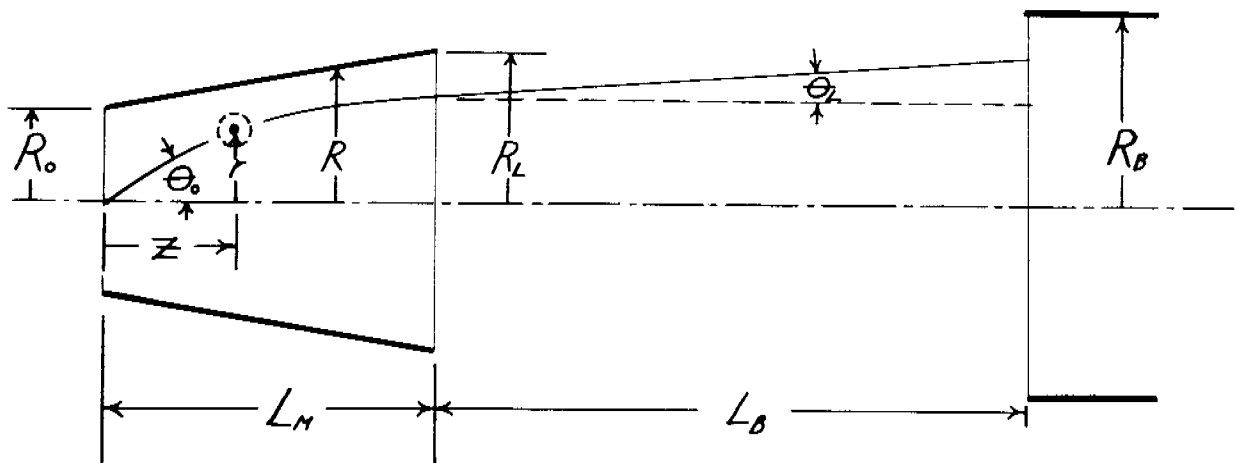


Figure 6. Diagram Of Coordinates And Parameters For Analysis Of Atom Trajectories Within State Selectors.

ATOM PATH IN QUADRUPOLE STATE SELECTOR  
FOR  $F(1, \pm 1)$  STATES OR  $F(\frac{1}{2}, 0)$  WITH  $H > H_c$

$$r_0 = 0, \quad R = R_0 + \alpha z, \quad \Theta_r^2 = \frac{\mu_0 H}{\frac{m}{2} v^2} = \Theta_w^2$$

$$\frac{J^2 r}{J z^2} + \frac{\Theta_r^2}{2R} = 0 \quad \begin{pmatrix} + \text{ATTRACTING} \\ - \text{DEFLECTING} \end{pmatrix}$$

$$r = \Theta_0 z + \frac{\Theta_r^2}{2\alpha^2} \left[ R \left\{ \ln \left( \frac{R}{R_0} \right) - 1 \right\} + R_0 \right]$$

$$\Theta = \Theta_0 + \frac{\Theta_r^2}{2\alpha} \ln \left( \frac{R}{R_0} \right)$$

AS  $\alpha \rightarrow 0$  (NO TAPER)

$$r = \left( \Theta_0 + \frac{\Theta_r^2 z}{4 R_0} \right) z, \quad \Theta = \Theta_0 + \frac{\Theta_r^2 z}{2 R_0}$$

Figure 7. Equations Of Motion Within State Selector For Cases Where The Magnetic Moment Is Constant, Or Nearly So.



ATOM PATH IN QUADRUPOLE STATE SELECTOR  
 FOR  $F(1,0/0,0)$  STATES ( $H < H_1$ ) OR HEXAPOLE  
 FOR  $F(1,\pm 1)$  STATES.  $r_0 = 0$ ,  $R = R_0 + \alpha z$

$$\Theta_w^2 = \frac{g_F H \Theta_T^2}{4 H_1} \quad (H < H_1, F(1,0/0,0))$$

$$\Theta_w^2 = \Theta_T^2 = \frac{\mu_0 H}{(\frac{m \hbar \omega}{2})} \quad (H > H_1 \text{ or } F(1,\pm 1))$$

---

ATTRACTING:  $\Phi_1 \equiv \beta_1 \ln(R/R_0)$ ,  $\beta_1 \equiv \sqrt{\frac{\Theta_w^2}{\alpha^2} - \frac{1}{4}}$

$$r = \frac{\Theta_0 \sqrt{R R_0}}{\beta_1} \sin \Phi_1, \quad \Theta = \frac{\Theta_0 \sqrt{R/R_0}}{2 \beta_1} [\sin \Phi_1 + 2 \beta_1 \cos \Phi_1]$$


---

DEFLECTING: Replace  $\sin$  With  $\sinh$ ,  $\cos$  With  $\cosh$   
 &  $\Phi_2 \equiv \beta_2 \ln(R/R_0)$ ,  $\beta_2 \equiv \sqrt{\frac{\Theta_w^2}{\alpha^2} + \frac{1}{4}}$

---

LIM  $\alpha \rightarrow 0$  ATT:  $r = r_{MAX} \sin \Phi_3$ ,  $\Theta = \Theta_0 \cos \Phi_3$   
 $\Phi_3 \equiv \Theta_w \frac{z}{R_0}$  DEF:  $r = r_{LMAX} \sinh \Phi_3$ ,  $\Theta = \Theta_0 \cosh \Phi_3$

---

Figure 8. Equations Of Motion Within Quadrupole State Selector For ( $m = 0$ ) Cases Where  $H$  Is Less Than  $H_1$  Or Within Hexapole In Cases Where The Magnetic Moment Is Constant, Or Nearly So.

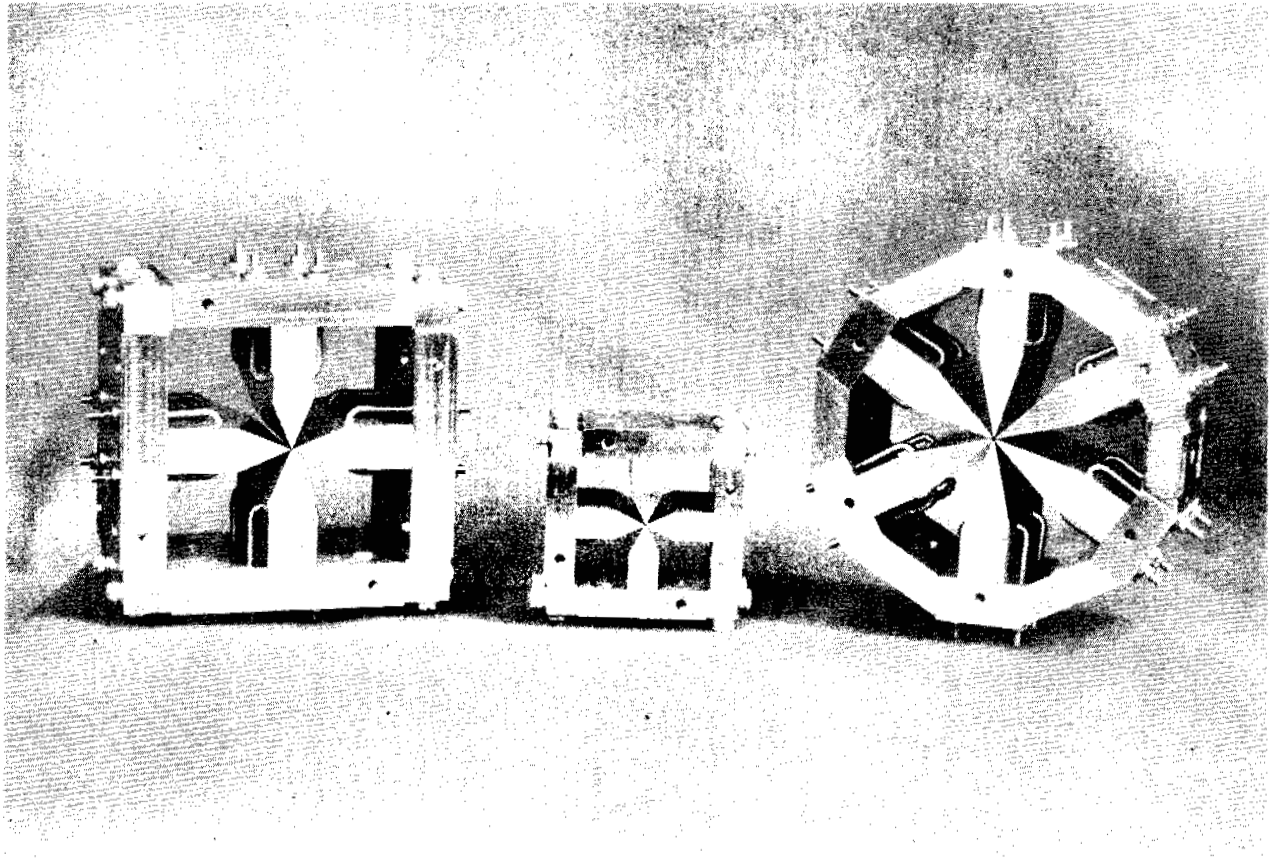


Figure 9. Quadrupole And Hexapole State Selectors Produced At Sigma Tau Standards Corporation. For Dimensional Reference The Small Quadrupole In The Center Has A Tapered Bore With Entrance Diameter of .46 mm, Exit Diameter .97 mm, And Is 25.4 mm Long. The Poles Are Saturated And Have Tip Fields Of Approximately 10 Kilogauss In The Quadrupole Units, And 7 Kilogauss In The Hexapole.

## QUESTIONS AND ANSWERS

DR. VICTOR REINHARDT, NASA/Goddard

What kind of efficiency improvement do you see in a tapered bore over a non-tapered bore? And how do you measure it?

MR. PETERS:

Okay. Well, if you use a quadrupole you'll get about a 50 percent efficiency in total solid angle. But if you also use a tapered bore of the right geometry, that is up to the saturate point and adjust it, the big end, and the small end is the proper dimensions, you'll get another factor of at least 50 percent, because in a hydrogen maser you are going to focus a lot more of the high velocity atoms, due to the intense fields near the source. It's an indeterminate increase in atoms over the case of a more conventional state selector.

Now over just a straight bore state selector, probably it would be something on the order of the small geometry. It'll probably be no more than a 50 percent difference.

I should mention that the straight geometry on a small bore state selector has an advantage for close up trajectories in that it defocusses all the wrong state atoms very effectively. And so, then, in some cases, you may still want to use a straight bore state selector.

DR. REINHARDT:

Have you experimentally verified that?

By looking at a hydrogen maser. Tapered bore versus straight bore.

MR. PETERS:

No, Victor, I haven't.

DR. REINHARDT:

Thanks a lot.

DR. WINKLER:

Your talk brought back memories of 1959 when Professor Kusch suggested very strongly in an analysis to use thallium. And from almost all points of view it would be a superior choice. Except that

work which then was started in a couple of laboratories was stopped because of the difficulty to detect it.

And now, of course, you could consider schemes of optical pumping and optical detection. And then that would be an entirely different situation. Have you thought about that?

MR. PETERS:

Yes, indeed, Dr. Winkler. I think that we can. Of course, the earlier schemes with thallium Zeeman transitions were to boot the one state down to the one zero state. And this has its advantages or disadvantages.

But if we can focus an intense, very intense beam of the one zero -- relatively, I should say, you lose about a factor of 12, but you gain by focussing the one zero state.

You can gain part of this back by selecting a lower temperature from the distribution. And this is done in cesium, for example. But, if you get a very intense beam, a relatively very intense beam, and you should be able to get, maybe, three or four orders of magnitude more atoms at the detector than you do with a cesium beam, which is only about 10 to the sixth, or 10 to the seventh, atoms per second, to get the marvelous performances they are getting.

You could use a modern mass spectrometer, commercially available, probably, to get the same signal to noise ratio.

You could probably use laser techniques. I think you might use a penning trap or another type of trap ionizer to ionize the thallium atoms.

So I think this problem could be solved. And it certainly deserves looking into.

DR. JOHN BERLINSKY, University of British Columbia

I didn't mention this, but in our low temperature experiments we make the RF discharge at the temperature of the dilution refrigerator, which is about half a degree.

And some of our competitors have demonstrated that you can make a beam where the nozzle at the outlet is at four degrees, and the beam temperature, the temperature distribution looks like a five degree distribution.

Our needs, on the other hand, are more or less the same as you described. We would like to have a small state selector with good acceptance.

How much could you improve things, if you could work the beam at low temperatures?

MR. PETERS:

I don't see -- well, of course I don't know exactly the design of state selector that you are presently acquainted with, or using.

DR. BERLINSKY:

Well, we don't, of course, in our present experiments use a state selector. But if we made a maser we might.

MR. PETERS:

Well, the only problem that I can see off-handedly, I haven't looked at the low temperature properties, the materials in the state selector in detail, it seems to me would be the thermal expansion coefficients between the cerium cobalt magnet parts and the soft iron parts. And I think they're all good materials and retain their magnetism, and it's far below the Curie point.

The small magnet you saw here used epoxy, which we'd probably have to do away with, and they can easily be fastened, just as the larger ones were, with screws and the adjustables. So I see no reason why that couldn't be applied.

Also I started to put together, but it was a little tedious, one which was only a half an inch long, and as small a bore diameter as I could realistically work with under the microscope. But I didn't bring it. I said in the program, perhaps, I was going to. But I didn't.

But this could give you one this big. And I don't know if you're worried about the proximity of the source to the region. But I suspect that within this range of sizes something would probably apply very realistically to your apparatus.

DR. REINHARDT:

One quick comment, to further answer that question.

Because the atoms are moving much slower at low temperature, your efficiency theoretically should go up as the ratio of the temperature.

MR. PETERS:

Oh, I forgot that. Yes, my yes.

DR. REINHARDT:

But I think the angles would get so large that you'd limit to two  $\pi$  solid angles.

DR. VESSOT:

Things look awfully good when things get cold, Victor. There's no question about it. And anything Harry said would apply in space.

MR. PETERS:

If I could answer that question further. I think that a tapered or curved pole state selector with a parabolic curve like a space antenna would probably do the job without any further calculations at the moment.

And it probably is very feasible. But your poles won't be saturated if you get a larger bore. You'll have to deal with a little bit different calculation.